Pressure in an exactly solvable model of active fluid

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We consider the pressure in the steady-state regime of three stochastic models characterized by self-propulsion and persistent motion and widely employed to describe the behavior of active particles, namely the Active Brownian particle (ABP) model, the Gaussian colored noise (GCN) model and the unified colored noise model (UCNA). Whereas in the limit of short but finite persistence time the pressure in the UCNA model can be obtained by different methods which have an analog in equilibrium systems, in the remaining two models only the virial route is, in general, possible. According to this method, notwithstanding each model obeys its own specific microscopic law of evolution, the pressure displays a certain universal behavior. For generic interparticle and confining potentials we derive a formula which establishes a correspondence between the GCN and the UCNA pressures. In order to provide explicit formulas and examples, we specialize the discussion to the case of an assembly of elastic dumbbells confined to a parabolic well. By employing the UCNA we find that, for this model, the pressure determined by the thermodynamic method coincides with the pressures obtained by the virial and mechanical methods. The three methods when applied to the GCN give a pressure identical to that obtained via the UCNA. Finally, we find that the ABP virial pressure exactly agrees with the UCNA and GCN result.

I. INTRODUCTION

The understanding of the properties of animated self-propelling agents is a challenge which recently attracted a profound interest in the condensed-matter physics community. Such systems commonly referred to as "active matter", are able to convert energy from the environment into directed persistent motion either by metabolic processes, as in the case of bacteria and spermatozoa, or by chemical reactions as in the case of synthetic Janus particles[1–4].

From the theoretical point of view, it is interesting to study the non-equilibrium steady-states (NESS), resulting from the balance between the energy continuously produced by the self-propulsion mechanism and the one consumed by dissipative forces exerted on the active particles by the viscous medium. It is natural to ask whether one can characterize the NESS according to few macroscopic observables such as temperature, pressure and chemical potential and construct a "thermodynamic" theory. A few years ago, Takatori et al.[5,6] discussed how to define and measure the pressure in active fluids and determined a new contribution to it stemming from the self-propulsion of the particles. They remarked that an assembly of such particles as a result of their activity would swim away unless confined by boundaries and identified the swimming pressure with the force per

unit area necessary to constrain them inside that region of space. The pressure problem has been recently tackled by statistical mechanics methods by especially considering two descriptions of active matter, namely the active Brownian particle (ABP) model[7–9] and Gaussian colored noise model (GCN)[10] characterized by different modeling of the active driving force. In the case of confined spherical ABP with torque-free wall and interparticle forces, Solon and coworkers[11] derived an expression for the mechanical pressure and proved that it is a state function independent of the wall interaction, while Winkler et al.[12] considered a virial method for ABP confined by solid walls or exposed to periodic boundary conditions. The pressure in the GCN model, instead, was recently studied by Fily et al.[13] and Sandford and Grosberg[14]. In the case of the GCN, one can further simplify the analysis by introducing a simplified model the so-called unified colored noise approximation (UCNA)[15,16]. A common ingredient to all these models is the presence of a persistence time τ which determines their special features, which do not have counterparts in equilibrium systems, such as the persistence of the trajectories of the particles, correlated motions and decrease of their mobility as the density increases. The UCNA[17] has the special property that its configurational steady state distribution is known, and that its pressure can be estimated by three different prescriptions mutually consistent in the limit of small but finite τ. These are: a) the Clausius virial method[18,19], b) a "thermodynamic" volume scaling method, which uses the volume derivative with respect to the system's volume of the partition function associated

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with the NESS distribution function and c) a method based on the evaluation of the work of deformation in terms of the microscopic pair correlation function.

Since exact results are scarce in this area, we consider instructive to tackle the pressure problem by applying different statistical methods to a minimal model for which, in many cases, we shall show, the analysis can be performed without approximations. The model was introduced by Riddell and Uhlenbeck (RU) a long time ago[20] to represent a collection of noninteracting particle pairs mutually connected by harmonic springs (elastic dumbbells) and confined by a harmonic trap. In spite of its simplicity, the RU model displays non trivial features, such as the mobility reduction induced by the interactions, a dependence of the pressure on the persistence time τ and on the strength of the couplings. One of the advantages of the RU model is the possibility to compute the pressure exactly within the GCN and the UCNA by the three methods above mentioned. The explicit UCNA calculation shows that the different determinations of the pressure coincide to all orders in τ and not only to first order as one can prove for the case of a generic potential. Interestingly, within the RU model such an equivalence between different determinations of the pressure holds exactly also for the GCN and the GCN and UCNA pressures are identical. On the other hand, concerning the ABP version of the RU model, we can only compute the pressure by the virial method and again we find that it has the same expression as the pressure of the GCN and UCNA models.

The paper is organized as follows: in section II, in order to allow the comparison between different treatments, we first introduce the ABP, GCN, and UCNA models in the case rather general interactions, establish the parameter correspondence among them and briefly review how to obtain the pressure in terms of steady-state statistical averages. In section III, we specialize the description and consider an application of our methods to the RU model. Finally, in section IV we come to the conclusions and perspectives. In order to limit the amount of mathematical details in the main text, we confined the technical aspects to three appendices.

II. ACTIVE PARTICLES MODELS AND THEIR PRESSURE

In the following, we consider the properties of an assembly of particles subjected to velocity dependent frictional forces due to a solvent, to conservative forces and to active forces. Such a description has been employed in the recent literature and contains the minimal ingredients necessary to reproduce the basic features of an active fluid. The following equation describes the evolution of the positions of a set of particles suspended in an active bath

$$\dot{\mathbf{r}}_i = \frac{1}{\gamma} \sum_k \boldsymbol{\Gamma}_{i,k}^{-1} \left[\mathbf{F}_k + \mathbf{A}_k \right] \qquad (1)$$

where i is the particle label and the matrix $\boldsymbol{\Gamma}$ represents a non dimensional friction matrix whose particular form depends on the model analyzed and will be specified below. Each particle is driven by a conservative force $\boldsymbol{F}_i = -\nabla_i \mathcal{U}$, an active force $\mathbf{A}_i$ and experiences a drag force, $-\gamma \dot{\mathbf{r}}_i$, with the solvent with drag coefficient γ. $\mathbf{A}_i$ is stochastic and correlated in time, τ being its characteristic time associated with the persistent motion. Equation (1) is rather general and can represent few different models commonly used in active matter according to which prescription is adopted for $\mathbf{A}_i$ and $\boldsymbol{\Gamma}$. We focus on three models, namely the Active Brownian Particle (ABP) model[21–23], the Gaussian colored noise (GCN)[24,25] or Active Ornstein-Uhlenbeck model and the unified colored noise approximation (UCNA) model[26]. The ABP model was proposed on a phenomenological basis to describe in terms of a set of stochastic differential equations containing a minimal set of parameters the observed behavior of active fluids and somehow originated the remaining two models. In fact, the GCN can be viewed as a simplified version of the ABP: it shares the same deterministic forces but is characterized by a Gaussian distribution of the active force $\mathbf{A}_i$ subject to the constraint of having the same variance and time correlation as its counterpart in the ABP. The UCNA, which is of interest because it lends itself to analytic treatments, can be regarded as an (approximated) reduction of the GCN to a Markovian form. Its dynamics is local in time but is characterized by effective non pairwise forces not present in the GCN and stemming from the elimination procedure of the fast degrees of freedom present in the GCN. The origin of these non pairwise forces is the presence of non-diagonal terms in the UCNA matrix $\boldsymbol{\Gamma}$ giving rise to an effective Hamiltonian involving, in principle, two, three, four up to N-particles interactions.

Both in the ABP and GCN models the friction matrix $\boldsymbol{\Gamma}$ has a very simple structure and is the identity $\mathbf{I}$. On the contrary, the friction matrix $\boldsymbol{\Gamma}$ is not diagonal in the UCNA and contains in addition to $\mathbf{I}$ the Hessian matrix of the potential $\mathcal{U}$, i.e. $\boldsymbol{\Gamma} = \mathbf{I} + \tau \mathbf{H}$, where the elements of $\mathbf{H}$ are $-\frac{1}{\gamma} \frac{\partial F_{\alpha i}}{\partial x_{\beta k}}$. In table I, for comparison, we report a synoptic view of the explicit form of the dynamic equation (1) in each model. The deterministic force $\boldsymbol{F}_i$ is assumed to be the same in each model. The third key ingredient is the active force $\mathbf{A}_i = \gamma v_0 \mathbf{e}_i$. As also illustrated in table I the active force $\mathbf{A}_i$ in the ABP is modeled by a vector of constant intensity γv_0, where v_0 is the propulsion speed, and random orientation, $\mathbf{e}_i$, performing a diffusive motion, on the unit sphere (or on the unit circle in $d = 2$) with rotational diffusivity constant D_r. The study of such a process involves the probability distribution not only of the positions, but also of the angles. The ABP micro-state, μ, in three dimensions is specified by N positions and $2N$ angles ($\mu = \{\mathbf{r}_i, \theta_i, \phi_i\}$

) and the angular dynamics is

$$\dot{\theta}_i(t) = D_r \cot \theta_i + \sqrt{D_r}\eta_i^\theta$$
$$\dot{\phi}_i(t) = \frac{\sqrt{D_r}}{\sin \theta_i}\eta_i^\phi(t). \qquad (2)$$

In two dimensions instead one needs only N angles θ_i evolving as:

$$\dot{\theta}_i(t) = \sqrt{D_r}\eta_i^\theta(t) \qquad (3)$$

and the micro-state is $\mu = \{\mathbf{r}_i, \theta_i\}$. The noises have zero average and correlations $\langle \eta_i^\theta(t)\eta_j^\theta(t')\rangle = 2\delta_{ij}\delta(t - t')$. If one uses the orientations, instead of the angles, it is easy to show that $\mathbf{e}_i$ at two different instants t and t' are exponentially correlated

$$\langle \mathbf{e}_i(t)\mathbf{e}_j(t')\rangle = e^{-(d-1)D_r|t-t'|}\mathbf{1}\delta_{ij}. \qquad (4)$$

The Gaussian colored noise model (GCN) represents a convenient alternative to the ABP and has been introduced with the main motivation of simplifying the theoretical study of active fluids, because it releases the hard constraint of constant magnitude of the velocity. The idea is to eliminate the active ABP force, $\gamma v_0 \mathbf{e}_i$, in favor of a non-Markovian term $\gamma \boldsymbol{u}_i$ of characteristic memory time, τ, and whose governing equation is:

$$\dot{\boldsymbol{u}}_i(t) = -\frac{1}{\tau}\boldsymbol{u}_i(t) + \frac{D^{1/2}}{\tau}\boldsymbol{\eta}_i(t). \qquad (5)$$

In the GCN each component of $\boldsymbol{u}_i$ is allowed to fluctuate between $-\infty$ and ∞, according to a Gaussian distribution of zero average and variance D/τ. By an appropriate choice of the parameters τ and D one can establish a correspondence between the ABP and the GCN statistical properties. In the GCN, the diffusion coefficient D is related to the original parameters by $D = \frac{v_0^2}{d(d-1)D_r}$, while τ the persistence time is $\tau^{-1} = (d-1)D_r$ while the time self-correlation of the velocity is by construction exponentially decaying as eq. (4) and adjusted to reproduce the velocity self-correlation of the ABP. The GCN micro-state, $\mu = \{\mathbf{r}_i, \boldsymbol{u}_i\}$, of the system is the set of the positions and of the velocities of each particle.

Finally, the UCNA represents a further approximation, aimed to simplify the analytic work, and may be derived from the GCN: it is tantamount of performing an adiabatic approximation replacing the colored noise term by an effective Markovian white noise. Such an elimination procedure brings about a complicated structure of the equations of evolution for the particles coordinates, due to the presence of a friction matrix $\boldsymbol{\Gamma}$ which in principle couples the motion of all particles[16,26,27].

In the UCNA case, the evolution equation (1) of the particle positions $\mathbf{r}_1, \ldots, \mathbf{r}_N$, identifying the micro state μ, takes the following specific form:

$$\dot{r}_{\alpha i} \simeq \sum_{\beta k} \Gamma_{\alpha i, \beta k}^{-1}\left[\frac{1}{\gamma}F_{\beta k} + D^{1/2}\eta_{\beta k}(t)\right]. \qquad (6)$$

with

$$\Gamma_{\alpha i, \beta k} = \delta_{ik}\delta_{\alpha\beta} + \frac{\tau}{\gamma}\frac{\partial^2 \mathcal{U}}{\partial x_{\alpha i}\partial x_{\beta k}} = \delta_{ik}\delta_{\alpha\beta} - \frac{\tau}{\gamma}\frac{\partial F_{\alpha i}}{\partial x_{\beta k}}. \qquad (7)$$

where Greek indexes stand for Cartesian components. The stochastic terms $\boldsymbol{\eta}_i(t)$ are Gaussian and Markovian processes distributed with zero mean and moments $\langle \boldsymbol{\eta}_i(t)\boldsymbol{\eta}_j(t')\rangle = 2\mathbf{1}\delta_{ij}\delta(t - t')$. Equation (6) shows that the effective friction and the effective noise experienced by each particle depend on the coordinates of all other particles.

A. Virial pressure

We turn now to review the methods to determine the pressure in the above models. Since the methods are based on the knowledge of the NESS distribution functions, instead of using the stochastic differential equation (1), it is more convenient to use the associated Fokker-Planck equation (FPE) describing the evolution of the probability distribution function of the micro states, μ. For all cases studied in the present paper the FPE can be written as:

$$\frac{\partial}{\partial t}P(\mu, t) = \mathcal{L}_{FP}P(\mu, t) \qquad (8)$$

where the specific form of the Fokker-Planck operator $\mathcal{L}_{FP}$, the sum of a diffusive and a drift contribution, is given explicitly in the following. The average of an observable $\mathcal{O}(\mu)$ evolves according to

$$\frac{\partial}{\partial t}\langle \mathcal{O}(\mu, t)\rangle = \langle \mathcal{L}_{FP}^\dagger \mathcal{O}(\mu, t)\rangle \qquad (9)$$

where $\mathcal{L}_{FP}^\dagger$ is the adjoint operator of the Fokker-Planck operator $\mathcal{L}_{FP}$ and $\langle \mathcal{O}(\mu, t)\rangle \equiv \int d\mu P(\mu, t)\mathcal{O}(\mu)$.

1. Virial pressure in the ABP and GCN models

To determine the pressure we employ the virial method [12,28] to obtain the virial of the forces. In $d = 3$ the ABP evolution equation for a generic operator $\mathcal{O}(\mathbf{r}_i, \theta_i, \phi_i)$ reads:

Stochastic dynamics of different active models					
Model	$\boldsymbol{\Gamma}_{i,k}$	$\mathbf{A}_i$	Active dynamics	Active noise Correlations	Diffusivity
ABP3	$\mathbf{I}_{i,k}$	$\gamma v_0 \mathbf{e}_i(t)$	$\dot{\theta}_i(t) = D_r \cot \theta_i + \sqrt{D_r}\eta_i^\theta$ $\dot{\phi}_i(t) = \frac{\sqrt{D_r}}{\sin\theta_i}\eta_i^\phi(t)$	$\langle \mathbf{e}_i(t)\mathbf{e}_j(t')\rangle = e^{-2D_r|t-t'|}\mathbf{1}\delta_{ij}$	$2D_r = 1/\tau$
ABP2	$\mathbf{I}_{i,k}$	$\gamma v_0 \mathbf{e}_i(t)$	$\dot{\theta}_i(t) = \sqrt{D_r}\eta_i^\theta(t)$	$\langle \mathbf{e}_i(t)\cdot \mathbf{e}_j(t')\rangle = e^{-D_r|t-t'|}\delta_{ij}$	$D_r = 1/\tau$
GCN	$\mathbf{I}_{i,k}$	$\gamma \boldsymbol{u}_i(t)$	$\dot{\boldsymbol{u}}_i(t) = -\frac{1}{\tau}\boldsymbol{u}_i(t) + \frac{D^{1/2}}{\tau}\boldsymbol{\eta}_i(t)$	$\langle \boldsymbol{u}_i(t)\,\boldsymbol{u}_j(t')\rangle = \frac{D}{\tau}e^{-|t-t'|/\tau}\mathbf{1}\delta_{ij}$	$D = \frac{v_0^2}{d(d-1)D_r}$
UCNA	$\delta_{ik}\delta_{\alpha\beta} + \frac{\tau}{\gamma}\frac{\partial^2 \mathcal{U}}{\partial x_{\alpha i}\partial x_{\beta k}}$	$\gamma D^{1/2}\boldsymbol{\eta}_i(t)$	$\boldsymbol{\eta}_i(t)$ is a Wiener process	$\langle \boldsymbol{\eta}_i(t)\boldsymbol{\eta}_j(t')\rangle = 2\boldsymbol{\delta}_{ij}\delta(t-t')$	D

TABLE I. Comparison between the stochastic dynamics describing the ABP in 3 and 2 dimensions, the GCN and the UCNA. For each model, in the second column we report the effective friction matrix $\boldsymbol{\Gamma}$, in the third column the active force $\mathbf{A}$, in the fourth we specify the stochastic equation associated with the active driving, in the fifth column we display the noise correlations and in the sixth the diffusivity of each model.

$$\frac{d\langle \mathcal{O}(t)\rangle^{ABP}}{dt} = \int d^N\mathbf{r} \int_0^{2\pi} d^N\phi \int_0^\pi d^N\theta \sin\theta\, P_N^{ABP}(\mathbf{r}_i,\theta_i,\phi_i,t) \sum_i \Big(\frac{1}{\gamma}(\boldsymbol{F}_i + \mathbf{A}_i)\frac{\partial}{\partial \mathbf{r}_i}$$
$$+ D_r\Big(\frac{1}{\sin\theta_i}\frac{\partial}{\partial \theta_i}\sin\theta_i\frac{\partial}{\partial\theta_i} + \frac{1}{\sin^2\theta_i}\frac{\partial^2}{\partial\phi_i^2}\Big)\Big)\mathcal{O}(\mathbf{r}_i,\theta_i,\phi_i) \tag{10}$$

with $\mathbf{A}_i = \gamma v_0 \mathbf{e}_i$.

On the other hand, in the GCN model the evolution equation for $\mathcal{O}(\mathbf{r}_i,\boldsymbol{u}_i)$ is:

$$\frac{d\langle \mathcal{O}(t)\rangle^{GCN}}{dt} = \int d^N\mathbf{r} \int d^N\boldsymbol{u}\, P_N^{GCN}(\mathbf{r}_i,\boldsymbol{u}_i,t) \sum_i \Big(\frac{1}{\gamma}(\boldsymbol{F}_i + \mathbf{A}_i)\frac{\partial}{\partial \mathbf{r}_i} - \frac{\boldsymbol{u}_i}{\tau}\frac{\partial}{\partial \boldsymbol{u}_i} + \frac{D}{\tau^2}\frac{\partial^2}{\partial \boldsymbol{u}_i^2}\Big)\mathcal{O}(\mathbf{r}_i,\boldsymbol{u}_i) \tag{11}$$

and $\mathbf{A}_i = \gamma \mathbf{u}_i$. The virial of the forces is obtained by choosing $\mathcal{O} = \sum_i \mathbf{r}_i \cdot \mathbf{r}_i$, that is the mean square displacement of the particles with respect to the origin. Its average is asymptotically bounded by the presence of the walls and its derivative vanishes as for $t \to \infty$. In both models, one obtains the following equation, relating the virial of the external forces $-p_v dL^d = \sum_i^N \langle \boldsymbol{F}_i^{ext} \cdot \mathbf{r}_i\rangle$ to the internal virial $\frac{1}{2}\sum_{i\neq j}\langle \boldsymbol{F}_{ij} \cdot (\mathbf{r}_i - \mathbf{r}_j)\rangle$ and to the average of the moment arm of the active force $\langle \mathbf{A}_i \cdot \mathbf{r}_i\rangle$:

$$p_v V L^d = \frac{1}{2}\sum_{i\neq j}\langle \boldsymbol{F}_{ij} \cdot (\mathbf{r}_i - \mathbf{r}_j)\rangle + \sum_i \langle \mathbf{A}_i \cdot \mathbf{r}_i\rangle. \tag{12}$$

Eq. (12) is not a closed equation because the ABP and GCN not only require the knowledge of the probability distribution of the particle positions, but also of the correlations between these and the active forces $\mathbf{A}_i$. Thus, we need to consider the evolution of the average of the operators $\mathcal{O} = \mathbf{r}_i \cdot \mathbf{e}_i$ and $\mathcal{O} = \mathbf{r}_i \cdot \boldsymbol{u}_i$, in the case of the ABP and GCN, respectively. In both instances, we can write an auxiliary equation under the same form:

$$\frac{\gamma}{\tau}\sum_i \langle \mathbf{A}_i \cdot \mathbf{r}_i\rangle = NdD\frac{\gamma^2}{\tau} + \sum_i \langle \boldsymbol{F}_i^{ext} \cdot \mathbf{A}_i\rangle +$$
$$\frac{1}{2}\sum_{i\neq j}\langle \boldsymbol{F}_{ij} \cdot (\mathbf{A}_i - \mathbf{A}_j)\rangle, \tag{13}$$

where we have used the correspondence relations $\tau^{-1} = (d-1)D_r$ and $D = \frac{v_0^2}{d(d-1)D_r}$ of table I in order to stress the similarity. The expression for the ABP and GCN pressure is obtained from (12), where the r.h.s. represents the internal pressure, whose form is reported for each case in the second column of table II, whereas the third column reports the corresponding form of the auxiliary equation (13). In the GCN case, we may derive in the small τ limit a closed equation for the steady-state average $\langle \mathbf{A}_i \cdot \mathbf{r}_i\rangle$, as shown in appendix A, whereas in the ABP we could obtain an explicit result only for a specific model comprising harmonic forces (see subsection III B 4).

2. Virial pressure in the UCNA

In the case of general potentials, the UCNA formulas for the pressure were derived in detail in ref.[17]: the virial pressure was shown to have the form:

$$p_v V d = \frac{1}{2}\sum_{i\neq j}\langle \boldsymbol{F}_{ij} \cdot (\mathbf{r}_i - \mathbf{r}_j)\rangle + D\gamma \sum_{\alpha i}\langle \Gamma_{\alpha i,\alpha i}^{-1}\rangle \tag{14}$$

Virial pressure		
Model	Internal pressure $p_v dL^d$	Auxiliary equation
ABP3	$\frac{1}{2}\sum'_{ij}\langle\boldsymbol{F}_{ij}\cdot(\mathbf{r}_i-\mathbf{r}_j)\rangle+\gamma v_0\sum_i\langle\mathbf{e}_i\cdot\mathbf{r}_i\rangle$	$\sum_i\langle\mathbf{e}_i\cdot\mathbf{r}_i\rangle=N\tau v_0+\frac{\tau}{\gamma}[\sum_i\langle\boldsymbol{F}_i^{ext}\cdot\mathbf{e}_i\rangle+\frac{1}{2}\sum'_{ij}\langle\boldsymbol{F}_{ij}\cdot(\mathbf{e}_i-\mathbf{e}_j)\rangle]$
ABP2	$\frac{1}{2}\sum'_{ij}\langle\boldsymbol{F}_{ij}\cdot(\mathbf{r}_i-\mathbf{r}_j)\rangle+\gamma v_0\sum_i\langle\mathbf{e}_i\cdot\mathbf{r}_i\rangle$	$\sum_i\langle\mathbf{e}_i\cdot\mathbf{r}_i\rangle=N\tau v_0+\frac{\tau}{\gamma}\sum_i[\langle\boldsymbol{F}_i^{ext}\cdot\mathbf{e}_i\rangle+\frac{1}{2}\sum'_{ij}\langle\boldsymbol{F}_{ij}\cdot(\mathbf{e}_i-\mathbf{e}_j)\rangle]$
GCN	$\frac{1}{2}\sum_{ij}\langle\boldsymbol{F}_{ij}\cdot(\mathbf{r}_i-\mathbf{r}_j)\rangle+\gamma\sum_i\langle\boldsymbol{u}_i\cdot\mathbf{r}_i\rangle$	$\sum_i\langle\boldsymbol{u}_i\cdot\mathbf{r}_i\rangle=NdD+\frac{\tau}{\gamma}[\sum_i\langle\boldsymbol{F}_i^{ext}\cdot\boldsymbol{u}_i\rangle+\frac{1}{2}\sum'_{ij}\langle\boldsymbol{F}_{ij}\cdot(\boldsymbol{u}_i-\boldsymbol{u}_j)\rangle]$
UCNA	$\frac{1}{2}\sum'_{ij}\langle\boldsymbol{F}_{ij}\cdot(\mathbf{r}_i-\mathbf{r}_j)\rangle+D\gamma\sum_{\alpha i}\langle\Gamma^{-1}_{\alpha i,\alpha i}\rangle$	$\sum_{\alpha i}\langle\Gamma^{-1}_{\alpha i,\alpha i}\rangle=\langle Tr[\mathbf{I}+\tau\mathbf{H}]^{-1}\rangle$

TABLE II. For each model, in the second column we display the contribution to the pressure due to the internal forces and to the diffusive dynamics. In the third column we report the auxiliary equation (given in the main text as eq. (13) for ABP and GCN, and as eq. (A1) for the UCNA) needed to obtain a closed expression for the pressure.

with $\sum_j\boldsymbol{F}_{ij}\equiv\sum_j\boldsymbol{F}^{particles}(\mathbf{r}_i-\mathbf{r}_j)=\boldsymbol{F}^{int}(\mathbf{r}_i)$ and $\Gamma^{-1}_{\alpha i,\beta j}=\left[\delta_{ij}\delta_{\alpha\beta}-\frac{\tau}{\gamma}\frac{\partial F^{ext}_{\alpha i}}{\partial r_{\beta j}}-\frac{\tau}{\gamma}\frac{\partial F^{int}_{\alpha i}}{\partial r_{\beta j}}\right]^{-1}$. The first term in eq. (14) is the analog of the non ideal pressure contribution in a passive fluid, whereas the second term represents the swim pressure.

One may observe the similarity between eqs. (12) and (14): the pressure is given by a direct interaction term involving pair forces and analogous to the contribution to the pressure of passive fluids stemming from the pair potential plus a term due to the presence of active forces. In appendix A, we shall show that the second terms featuring in the GCN (12) and UCNA (14) pressure equations are equivalent to first order in τ.

B. Thermodynamic and Mechanical determinations of the pressure

To first order in the non equilibrium parameter τ, two alternative procedures to measure the pressure in active systems[17] may also be applied: the first of these is a "thermodynamic" method. Let us suppose that we are able to determine the non-equilibrium steady-state distribution of micro-states, μ, and its normalizing factor, Z. We may identify Z with the relevant partition function and the pressure with its logarithmic derivative with respect to the volume times the temperature. In reference[17] it was verified that within the UCNA up to first order in τ such a "thermodynamic" pressure coincides with the virial pressure.

The second alternative procedure consists of a mechanical method to measure the pressure and employs the concept of work involved to increase the volume of the system and relates the force necessary to perform it to the microscopic structure of the system[29,30]. One takes advantage of the fact that the mechanical work associated with a strain, resulting from a nonuniform displacement of the particles of the fluid, can be expressed either in terms of the external force field which produces it or in terms of the product of the stress and strain tensors. Using the information contained in the microscopic distribution one and two-particles distribution functions one can determine the mechanical work and finally the pressure.

III. APPLICATION TO THE RIDDELL-UHLENBECK ACTIVE PARTICLES MODEL

In general, for given confining and inter-particle potentials it is not possible to write explicitly the pressure in terms of its control variables and to compare its expressions derived by different methods in order to verify their compatibility. As we discussed above the comparison shows an agreement to first order in τ, but it is difficult to go beyond for an arbitrary choice of potentials. In the following, in order to compare the pressure of different methods and different descriptions of the active forces, we shall employ an explicitly soluble model. The system is represented by N mutually noninteracting elastic dumbbells, i.e. two point particles bound together by an elastic spring of constant α^2, moving in a vessel represented by a harmonic weak confining potential, of spring constant ω^2. Such a model, similar to the harmonic trap model[10,31,32], was proposed long ago by Riddell and Uhlenbeck. It contains the minimal ingredients to observe the competition between internal forces and confining potential and can be solved without introducing further approximations. The RU[20] potential energy reads:

$$\mathcal{U}(\mathbf{r}_1,\mathbf{r}_2)=w(\mathbf{r}_1-\mathbf{r}_2)+u(\mathbf{r}_1)+u(\mathbf{r}_2)$$

with $w(\mathbf{r})=\frac{1}{2}\alpha^2\mathbf{r}^2$. By setting $u(\mathbf{r})=\frac{k}{2}\frac{\mathbf{r}^2}{L^2}$, one introduces a volume dependence in the spring constant associated with the confining potential and for simplicity of notation we shall use $\omega^2=\frac{k}{L^2}$. Provided the condition $-\alpha^2<\omega^2/2$ is satisfied, it is also possible to include the case of repulsive inter-particle quadratic potentials, which have been used in simulations of active particles[23]. We follow this strategy: for each of the three models, we derive, when possible, the pressure formula. In the UCNA and GCN cases, we apply the three routes and verify that the results of each case coincide, whereas in the ABP case we are able to obtain the pressure only via the virial route, but we show that the pressure is the same as the other six cases.

A. UCNA analysis of the Riddell-Uhlenbeck active model

By the adiabatic elimination of the velocities we obtain the corresponding approximate UCNA equations (1) . These equations are more conveniently written in terms of the "collective" coordinates $\mathbf{q} = (\mathbf{r}_1 - \mathbf{r}_2)$ and $\mathbf{Q} = (\mathbf{r}_1 + \mathbf{r}_2)/2$ and of the renormalised spring constant $\Omega^2 = \omega^2 + 2\alpha^2$ as:

$$\dot{\mathbf{q}} = -\frac{1}{1 + \frac{\tau}{\gamma}\Omega^2}\left(\frac{1}{\gamma}\Omega^2\mathbf{q} + D^{1/2}(\boldsymbol{\eta}_1 - \eta_2)\right) \quad (15)$$

$$\dot{\mathbf{Q}} = -\frac{1}{1 + \frac{\tau}{\gamma}\omega^2}\left(\frac{1}{\gamma}\omega^2\mathbf{Q} + D^{1/2}\frac{(\boldsymbol{\eta}_1 + \boldsymbol{\eta}_2)}{2}\right) \quad (16)$$

1. Thermodynamic route to the pressure

It is quite straightforward to obtain the steady-state non-equilibrium distribution function of the UCNA model. It reads:

$$P(\mathbf{q}, \mathbf{Q}) =$$
$$\frac{1}{Z}\exp\left\{-\beta[\omega^2(1 + \frac{\tau}{\gamma}\omega^2)\mathbf{Q}^2 + \frac{1}{4}\Omega^2(1 + \frac{\tau}{\gamma}\Omega^2)\mathbf{q}^2]\right\}\det\Gamma \quad (17)$$

where we used the abbreviations $1/\beta = D\gamma$ and $\det\Gamma = (1 + \frac{\tau}{\gamma}\omega^2)^d(1 + \frac{\tau}{\gamma}\Omega^2)^d$. Integrating over $\mathbf{q}$ and $\mathbf{Q}$ we obtain the "partition function" of the UCNA model:
$Z = 2\pi\frac{\left((1 + \frac{\tau}{\gamma}\omega^2)(1 + \frac{\tau}{\gamma}\Omega^2)\right)^{d/2}}{(\beta\omega\Omega)^d}$ and identify the logarithmic volume derivative of the partition function with a thermodynamic pressure :

$$p_t = \frac{1}{\beta}\frac{\partial}{\partial L^d}\ln Z = \frac{D\gamma}{L^d}\left\{\frac{1}{1 + \frac{\tau}{\gamma}\omega^2} + \frac{\omega^2}{\Omega^2}\frac{1}{1 + \frac{\tau}{\gamma}\Omega^2}\right\} \quad (18)$$

In Fig. 1 we show the behavior of p_t given by equation (18) as a function of τ. We normalized $p_t(\tau)$ with the value $p(0) = p_{eq}$, where p_{eq} it the equilibrium value of the pressure of an ideal gas of elastic dumbbells. The different curves refer to different values of $k = 0.1, 0.5, 1.0, 5, 10$. The remaining parameters are fixed to one, i. e., $L = \gamma = \alpha = D = 1$. As one can see the pressure monotonically decreases with τ and $\lim_{\tau\to\infty} p_t = 0$ when D is kept fixed.

2. Clausius Virial pressure in the UCNA model

The virial pressure is obtained by applying the general formula (14) with the choice $\mathcal{O} = \frac{1}{2}\sum_{ij}\sum_\alpha \Gamma_{ij}r_{\alpha i}r_{\alpha j}$:

$$p_v dL^d = -\langle \boldsymbol{F}_1^{ext}\cdot\mathbf{r}_1 + \boldsymbol{F}_2^{ext}\cdot\mathbf{r}_2\rangle = dD\gamma(\Gamma_{11}^{-1} + \Gamma_{22}^{-1}) + \langle \boldsymbol{F}_{12}\cdot(\mathbf{r}_1 - \mathbf{r}_2)\rangle. \quad (19)$$
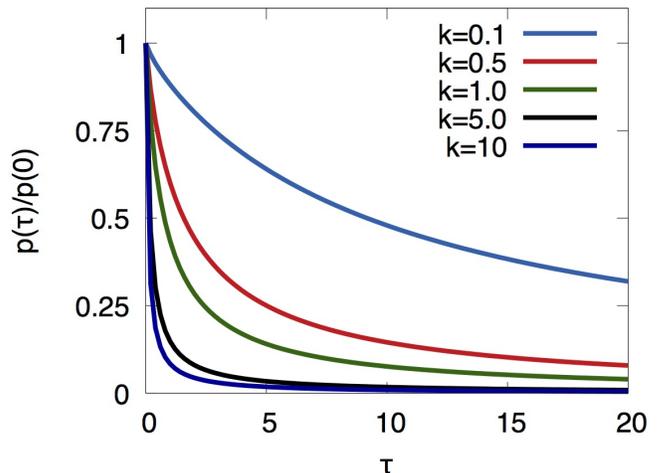

FIG. 1. Pressure as a function of τ for different values of $k = 0.1, 0.5, 1.0, 5.0, 10$ (blue,red,green,black, and dark blue, respectively) and $L = \gamma = \alpha = 1$.

Using the results $\Gamma_{11}^{-1} + \Gamma_{22}^{-1} = \frac{1}{1 + \frac{\tau}{\gamma}\omega^2} + \frac{1}{1 + \frac{\tau}{\gamma}\Omega^2}$ and $\langle\boldsymbol{F}_{12}\cdot(\mathbf{r}_1 - \mathbf{r}_2)\rangle = \frac{D\gamma}{\Omega^2}\frac{\omega^2 - \Omega^2}{1 + \frac{\tau}{\gamma}\Omega^2}$ we find $p_v = p_t$ and conclude that the mechanical pressure and the thermodynamic pressure are equal for this model. Notice that as $\alpha\to\infty$ the pressure of the dumbbell gas is only one-half of the pressure of a system of noninteracting particles contained in the same vessel, since each dumbbell behaves as a single particle.

3. Mechanical pressure in the UCNA model

We have recently shown[27] that within the UCNA it is possible to derive an exact hierarchy of equations, similar to the Born-Green-Yvon equations, connecting the distribution function, $P_N^{(m)}(\mathbf{r}_1, \ldots, \mathbf{r}_m)$, of m particles, in systems containing N of them, to those of $m' > m$ particles. As shown in appendix B we find that within the UCNA the virial, thermodynamic and distribution function route to computing the pressure give the same result, i.e. $p_v = p_t = p_V$ as in the case of equilibrium systems.

B. Riddell-Uhlenbeck model with Gaussian colored noise and for Active Brownian particles

We turn, now, to the study of the pressure in the RU model when the dynamics follow the GCN or the ABP prescription. The coordinates of the two particles evolve

according to the following equations :

$$\dot{\mathbf{r}}_1 = -\frac{1}{\gamma}\left(\omega^2\mathbf{r}_1 + \alpha^2(\mathbf{r}_1 - \mathbf{r}_2) - \mathbf{A}_1(t)\right) \quad (20)$$

$$\dot{\mathbf{r}}_2 = -\frac{1}{\gamma}\left(\omega^2\mathbf{r}_2 - \alpha^2(\mathbf{r}_1 - \mathbf{r}_2) - \mathbf{A}_2(t)\right) \quad (21)$$

The GCN corresponds to the choice $\mathbf{A}_i = \gamma\boldsymbol{u}_i(t)$ with: $\dot{\boldsymbol{u}}_i(t) = -\frac{1}{\tau}\boldsymbol{u}_i(t) + \frac{D^{1/2}}{\tau}\boldsymbol{\eta}_i(t)$, whereas the ABP to $\mathbf{A}_i = \gamma v_0 \mathbf{e}_i(t)$, where the unit vectors $\mathbf{e}_i$ identified by their angles evolve according to (2) and (3) in three and two dimensions, respectively.

1. RU+GCN model: virial route

We consider first the GCN case and derive the pressure by the virial and thermodynamic method. We show that within the GCN the virial expression of the pressure gives the same result as (18) by computing the stationary averages by integrating equations (20) and (21). in d dimensions we rewrite the virial equation appearing in the table II as:

$$p_v dL^d = -\sum_i^2 \langle \boldsymbol{F}_i^{ext} \cdot \mathbf{r}_i \rangle = -\alpha^2 \langle (\mathbf{r}_1 - \mathbf{r}_2)^2 \rangle + \gamma \sum_i \langle \boldsymbol{u}_i \cdot \mathbf{r}_i \rangle \quad (22)$$

The average of the operator $\mathcal{O} = \sum_i \boldsymbol{u}_i \cdot \mathbf{r}_i$ in the limit of $t \to \infty$ reads:

$$-\frac{1}{\gamma}\sum_i \langle \boldsymbol{F}_1^{ext} \cdot \boldsymbol{u}_1 \rangle = -\frac{\alpha^2}{\gamma}\langle (\mathbf{r}_1 - \mathbf{r}_2) \cdot (\boldsymbol{u}_1 - \boldsymbol{u}_2) \rangle -$$

$$\sum_i \frac{1}{\tau}\langle \boldsymbol{u}_i \cdot \mathbf{r}_i \rangle + \sum_i \langle \boldsymbol{u}_i \cdot \boldsymbol{u}_i \rangle \quad (23)$$

where the last term is given by $2dD/\tau$, and $\langle (\mathbf{r}_1 - \mathbf{r}_2) \cdot (\boldsymbol{u}_1 - \boldsymbol{u}_2) \rangle = \frac{Dd}{1+\frac{\tau}{\gamma}\Omega^2}$. After rearranging we find $\sum_i \langle \boldsymbol{u}_i \cdot \mathbf{r}_i \rangle = dD\left(\frac{1}{1+\frac{\tau}{\gamma}\omega^2} + \frac{1}{1+\frac{\tau}{\gamma}\Omega^2}\right)$ and using the result $\langle (\mathbf{r}_1 - \mathbf{r}_2)^2 \rangle = \frac{2d}{\Omega^2}\frac{D\gamma}{1+\frac{\tau}{\gamma}\Omega^2}$ we see that the virial pressure, p_v, of the GCN model coincides with formula (18) which was obtained by the UCNA method. Notice that the r.h.s. of eq. (22) displays the characteristic structure of the pressure in active systems. The first term is negative and contains the contribution to the pressure stemming from two-particle direct interactions, while the second represents the combination of the ideal and active contributions to the pressure.

2. RU+GCN model: thermodynamic route

In order to apply the "thermodynamic' route, we consider the following system of Markovian processes and recast (20) and (21) in terms of the collective coordinates q, Q:

$$\dot{q} = v \quad (24)$$

$$\dot{Q} = V \quad (25)$$

$$\dot{v} = -\frac{1}{\gamma}\Omega^2 v - \frac{v}{\tau} - \frac{\Omega^2}{\gamma\tau}q + \frac{D^{1/2}}{\tau}\sqrt{2}\eta_q \quad (26)$$

$$\dot{V} = -\frac{1}{\gamma}\omega^2 V - \frac{V}{\tau} - \frac{\omega^2}{\gamma\tau}Q + \frac{D^{1/2}}{\tau}\frac{1}{\sqrt{2}}\eta_Q, \quad (27)$$

By using the method illustrated in appendix C we obtain the following expression for the probability distribution of the coordinates q, Q:

$$P_c^{config}(q, Q) = \frac{1}{Z}\exp\left\{-\frac{\omega^2 Q^2(1+\frac{\tau}{\gamma}\omega^2) + \frac{\Omega^2}{4}q^2(1+\frac{\tau}{\gamma}\Omega^4)}{D\gamma}\right\}(1+\frac{\tau}{\gamma}\omega^2)(1+\frac{\tau}{\gamma}\Omega^2). \quad (28)$$

The normalizing factor Z is identical to the one already found in the UCNA treatment and also the "thermodynamic pressure" $\beta p_t = \frac{\partial}{\partial L}\ln Z$ is the same as (18). Let us remark that the above results can be easily extended to the d dimensional case by substituting $(q, Q) \to (\mathbf{q}, \mathbf{Q})$ and the factor $(1+\frac{\tau}{\gamma}\omega^2)(1+\frac{\tau}{\gamma}\Omega^2) \to (1+\frac{\tau}{\gamma}\omega^2)^d(1+\frac{\tau}{\gamma}\Omega^2)^d$.

3. RU+GCN model: distribution functions approach

In order to establish the equivalence between the pressure derived by the distribution functions approach and the virial and thermodynamic methods in the framework of the RU+GCN model we verified that the form P_c^{config} (28) satisfies the balance equation (B1), by using the form of the equations (C3) and (C4) . Thus we conclude even

in the GCN, the pressure computed by the distribution function approach is identical to the pressure of the virial method and, perhaps more interestingly, the GCN and the UCNA give identical results.

4. Virial pressure in the ABP model

We finally compute the pressure for the ABP model using the virial approach. This is the only example where we are able to give an explicit representation of the pressure in ABP systems. Let us consider the following equations of evolution

$$\dot{\mathbf{q}} = -\frac{1}{\gamma}\Omega^2\mathbf{q} + v_0\mathbf{e}_q \qquad (29)$$

$$\dot{\mathbf{Q}} = -\frac{1}{\gamma}\omega^2\mathbf{Q} + v_0\mathbf{e}_Q \qquad (30)$$

with $\mathbf{e}_q = \mathbf{e}_1 - \mathbf{e}_2$ and $\mathbf{e}_Q = \frac{(\mathbf{e}_1+\mathbf{e}_2)}{2}$. By applying the virial formula (12) we find

$$p_v V d = -\alpha^2\langle\mathbf{q}^2\rangle + \gamma v_0\frac{\langle\mathbf{e}_q\mathbf{q} + 4\mathbf{e}_Q\mathbf{Q}\rangle}{2} \qquad (31)$$

and after computing the steady-state averages featuring in the r.h.s. of eq. (31) with the help of eqs. (29), (30) and the relations $\langle\mathbf{e}_q\mathbf{q}\rangle = 2\frac{v_0\tau}{1+\frac{\tau}{\gamma}\Omega^2}$ and $\langle\mathbf{e}_Q\mathbf{Q}\rangle = \frac{1}{2}\frac{v_0\tau}{1+\frac{\tau}{\gamma}\omega^2}$ we find that the virial pressure for the RU+ABP model is given by a formula identical to eq. (18). Again we notice that the first term in the r.h.s. of eq. (31) is the virial of the interparticle forces, i.e. the so-called direct interaction term of the pressure, which has an analog in passive systems, while the second term is identified with the active pressure due to the diffusion of the particles and following the literature is named "swim virial"[5]. Such an explicit result is valid for arbitrary τ and relies on the linearity of the forces.

IV. CONCLUSIONS

In this paper, we have considered models of interacting active particles, characterized by different types of stochastic drivings, corresponding to ABP, GCN and UCNA dynamics. By focusing on the non-equilibrium steady-states of these models we have discussed in detail the notion of pressure, which by analogy with equilibrium systems can be derived (in some of the cases here investigated) from the analog of the partition function, from the virial theorem or from the calculation of the stress tensor. In particular, by considering an explicit model, that is a system of active elastic dumbbells confined by parabolic wells, we have found that the pressure in each model is the same independently from the differences in their dynamical evolution laws. In the case of the elastic dumbbells, the perfect agreement among different methods and different dynamical models holds

to all orders in τ and not only to first order, as predicted by the more general theory[17]. In the case of the UCNA, this can be understood as a consequence of the detailed balance condition which is implicitly assumed in the approximation[33]. The GCN, in general, does not enjoy of the detailed balance condition but in the case of harmonic forces, such a condition is satisfied. This is the reason why in the RU model the GCN and the UCNA pressure have the same value[33]. Finally, according to the virial method, the pressure in the RU+ABP model is the same as the two other models as the explicit solution shows, but the two remaining methods cannot be applied. Let us comment that the present results regarding the pressure of a gas of underdamped active dumbbells are different from those recently obtained by Joyeux and Bertin[8] for two reasons: we assumed overdamped dynamics and linear forces thus excluding any average torque acting locally on the dumbbells.

Appendix A: Equivalence between the active parts of the GCN and UCNA pressures

In the present appendix, we show the equivalence between the active pressure contribution obtained via the UCNA eq. (14):

$$\delta p^{UCNA} V d \equiv D\gamma \sum_{\alpha i}\langle\Gamma_{\alpha i,\alpha i}^{-1}\rangle =$$

$$D\gamma\left\langle Tr\left[\delta_{ij}\delta_{\alpha\beta} - \frac{\tau}{\gamma}\frac{\partial F_{\alpha i}^{ext}}{\partial r_{\beta j}} - \frac{\tau}{\gamma}\frac{\partial F_{\alpha i}^{int}}{\partial r_{\beta j}}\right]^{-1}\right\rangle \quad (A1)$$

and the one via the GCN, eq. (12):

$$\delta p^{GCN} V d \equiv \gamma\sum_i\langle\mathbf{u}_i \cdot \mathbf{r}_i\rangle =$$

$$NdD\gamma + \tau\left\langle\sum_i \boldsymbol{F}_i^{ext} \cdot \boldsymbol{u}_i + \frac{1}{2}\sum_{ij}'\boldsymbol{F}_{ij} \cdot (\boldsymbol{u}_i - \boldsymbol{u}_j)\right\rangle. \quad (A2)$$

Clearly, in the noninteracting case and with $\tau = 0$ the two formulas give the same active pressure $ND\gamma/V$. Hereafter, we show that to first order in τ (A1) and (A2) give the same contribution to the total pressure. By comparing the $\langle\boldsymbol{u}_i \cdot \mathbf{r}_i\rangle$ term in (A2) with $D\sum_\alpha\sum_i\langle\Gamma_{\alpha i,\alpha i}^{-1}\rangle$ term in (A1) and with the help of Novikov's theorem[34] we shall prove the equivalence. Let us consider the stochastic equation for the GCN model:

$$\frac{d\bar{x}_k(t)}{dt} = \frac{F_k(x)}{\gamma} + u_k(t), \qquad (A3)$$

where the index k stands for (α, i) and $x_k = r_{\alpha i}$. The Novikov theorem states that for a Gaussian process (with or without memory)[35,36] the average $\langle u_m(t)x_k(t)\rangle$ is given by:

$$\langle u_m(t)\Phi(u)\rangle = \int_0^t dt' c_{mm}(t,t')\left\langle\frac{\delta\Phi(u)}{\delta u_n}\right\rangle, \quad (A4)$$

where $\Phi(\{u\})$ denotes a function of the $\{u\}$, and $c_{mn}(t,t')$ is the time correlation function $c_{mn}(t,t') = \langle u_m(t)u_n(t')\rangle = \delta_{mn}\frac{D}{\tau}\exp(-\frac{|t-t'|}{\tau})$. In our case eq. (A4) becomes

$$\langle x_k(t)u_m(t)\rangle = \int_0^t dt' c_{mm}(t,t')\langle \frac{\delta x_k(t)}{\delta u_m(t')}\rangle \qquad (A5)$$

After integrating Eq. (A3), we get

$$\bar{x}_k(t) = x_k(0) + \int_0^t ds\,[\frac{F_k(\bar{x}(s))}{\gamma} + u_k(s)]. \quad (A6)$$

The functional derivative of $\bar{x}_k(t)$ with respect to $u_m(t')$ becomes

$$\frac{\delta \bar{x}_k(t)}{\delta u_m(t')} =$$
$$\delta_{km}\theta(t-t') + \int_{t'}^t ds\,\frac{1}{\gamma}\frac{\partial F_k(\{\bar{x}(s)\})}{\partial x_n(s)}\frac{\delta \bar{x}_n(s)}{\delta u_m(t')}. \quad (A7)$$

and the derivative of Eq. (A7) with respect to t is given by

$$\frac{\partial}{\partial t}\left[\frac{\delta \bar{x}_k(t)}{\delta u_m(t')}\right] =$$
$$\delta_{km}\delta(t-t') + \frac{1}{\gamma}\frac{\partial F_k(\{\bar{x}(t)\})}{\partial x_n(t)}\frac{\delta \bar{x}_n(t)}{\delta u_m(t')}. \qquad (A8)$$

Define, now, $H_{kn}(t) = -\frac{1}{\gamma}\frac{\partial F_k(\{x(t)\})}{\partial x_n(t)}$ and rewrite (A8) as:

$$\frac{\partial}{\partial t}\left[\frac{\delta \bar{x}_n(t)}{\delta u_m(t')}\right] = \delta_{mn}\delta(t-t') - H_{kn}(t)\frac{\delta \bar{x}_n(t)}{\delta u_m(t')}, (A9)$$

whose formal solution with the initial condition

$$\left[\frac{\delta \bar{x}_n(t)}{\delta u_m(t')}\right]_{t=t'} = \delta_{mn}, \qquad (A10)$$

is given (for $t > t'$) by

$$\frac{\delta \bar{x}_n(t)}{\delta u_m(t')} = \theta(t-t')\exp\left(-\int_{t'}^t ds\,\mathbf{H}(s)\right)_{nm}. (A11)$$

Combining eq. (A5) with eq. (A11), we get

$$\langle x_k(t)u_m(t)\rangle =$$
$$\int_0^t dt'\theta(t-t')c_{mm}(t,t')\left\langle \exp\left(-\int_{t'}^t ds\mathbf{H}(s)\right)_{km}\right\rangle. \quad (A12)$$

By a change variable $z \equiv (t-t')/\tau$ and substitution of the explicit expression of $c_{mm}(t,t')$, we obtain

$$\langle x_k(t)u_m(t)\rangle =$$
$$D\int_0^{t/\tau} dz\,\exp(-z)\left\langle \exp\left(-\int_{t-\tau z}^t ds\mathbf{H}(s)\right)_{km}\right\rangle. \quad (A13)$$

By taking the small τ limit, i.e. assuming that $\bar{x}_n$ does not vary significantly over the correlation time of the noise, we can express the integral in the exponent as

$$\int_{t-\tau z}^t ds\mathbf{H}(s) \approx \tau z\mathbf{H}(t) - \frac{1}{2}\frac{d\mathbf{H}(t)}{dt}\tau^2 z^2 + \ldots$$

Neglecting the quadratic term proportional to $\tau^2 z^2$ the explicit form of (A5) reads

$$\langle x_m(t)u_m(t)\rangle \approx D\left\langle \left(\mathbf{I} + \tau\mathbf{H}\right)^{-1}_{mm}\right\rangle \qquad (A14)$$

Finally, going back to the physical variables of interest we obtain the result

$$\gamma\sum_i\langle \mathbf{u}_i \cdot \mathbf{r}_i\rangle = \gamma\sum_k\langle u_k(t)x_k(t)\rangle =$$
$$D\gamma\left\langle \langle Tr\left[\delta_{ij}\delta_{\alpha\beta} - \frac{\tau}{\gamma}\frac{\partial F_{\alpha i}^{ext}}{\partial r_{\beta j}} - \frac{\tau}{\gamma}\frac{\partial F_{\alpha i}^{int}}{\partial r_{\beta j}}\right]^{-1}\right\rangle \quad (A15)$$

Thus, we have shown that the two expression for the active pressure, in GCN and UCNA models, coincide to first order in τ. Unfortunately, attempts to include the ABP model in this analysis are hampered by the non Gaussian nature of the noise distribution associated with the corresponding $u_n(t)$. Only in the case of linear forces it is possible to derive an explicit result for the pressure.

Appendix B: Mechanical pressure in the RU UCNA

The exact steady-state distribution function for $N = 2$ particles takes the simple form

$$-D\gamma\sum_\beta\sum_{j=1,2}\frac{\partial}{\partial r_{\beta j}}[\Gamma_{\alpha 1,\beta j}^{-1}(\mathbf{r}_1,\mathbf{r}_2)P_2(\mathbf{r}_1,\mathbf{r}_2)] =$$
$$P_2(\mathbf{r}_1,\mathbf{r}_2)\left(\frac{\partial u(\mathbf{r}_1)}{\partial r_{\alpha 1}} + \frac{\partial w(\mathbf{r}_1 - \mathbf{r}_2)}{\partial r_{\alpha 1}}\right). \qquad (B1)$$

Integrating both sides of equation (B1) with respect to $\mathbf{r}_2$ and recalling that $\mathbf{\Gamma}$ is constant for the oscillator problem we obtain

$$P_2^{(1)}(\mathbf{r}_1)F_\alpha^{ext}(\mathbf{r}_1)$$
$$= D\gamma\Gamma_{\alpha 1,\alpha 1}^{-1}\frac{\partial}{\partial r_{\alpha 1}}P_2^{(1)}(\mathbf{r}_1) + \int d\mathbf{r}_2 P_2(\mathbf{r}_1,\mathbf{r}_2)\frac{\partial w(\mathbf{r}_1 - \mathbf{r}_2)}{\partial r_{\alpha 1}}$$
$$(B2)$$

where $P_2^{(1)}(\mathbf{r}_1) \equiv \int d\mathbf{r}_2 P_2(\mathbf{r}_1,\mathbf{r}_2)$ is the marginalized one particle distribution function and $\mathbf{F}^{ext}(\mathbf{r}) = -\frac{\partial u(\mathbf{r})}{\partial \mathbf{r}}$. Following ref.[17] we now use eq. (B2) to derive an expression for the pressure in terms of the work of deformation, δW_F, necessary to produce a change of volume δV. We obtain δW_F by multiplying the l.h.s. of eq. (B2) by an infinitesimal displacement $\delta\mathbf{s}(\mathbf{r}) = \lambda\mathbf{r}$ and integrating over the volume:

$$\delta W_F = \int d^d\mathbf{r}\,\rho(\mathbf{r})\mathbf{F}^{\mathbf{ext}}(\mathbf{r}) \cdot \delta\mathbf{s}(\mathbf{r}) \qquad (B3)$$

where we introduced the particle density via $\rho(\mathbf{r}) = 2P_2^{(1)}(\mathbf{r})$. Using eq. (B2) we get

$$\delta W_F = -\lambda dD\gamma\Big(\frac{1}{1+\frac{\tau}{\gamma}\omega^2} + \frac{\omega^2}{\Omega^2}\frac{1}{1+\frac{\tau}{\gamma}\Omega^2}\Big) \qquad \text{(B4)}$$

On the other hand, one can evaluate the work of deformation as the integral over the volume of the trace of the product of the pressure tensor $p_{\alpha\beta}(\mathbf{r})$ times the strain tensor, $\delta\epsilon_{\alpha\beta}$, associated with the local displacement $\delta\mathbf{s}(\mathbf{r})$ of the fluid. With the help of the explicit formula $\delta\epsilon_{\alpha\beta} = \frac{1}{2}(\frac{\partial \delta s_\alpha}{\partial r_\beta} + \frac{\partial \delta s_\beta}{\partial r_\alpha}) = \lambda\delta_{\alpha\beta}$ such a work can be calculated as:

$$\delta W_p = -\int d\mathbf{r}\sum_{\alpha\beta} p_{\alpha\beta}(\mathbf{r})\delta\epsilon_{\alpha\beta}(\mathbf{r}) = -\lambda dL^d p_V \qquad \text{(B5)}$$

where p_V is the volume averaged pressure tensor. Since δW_F and δW_p must be equal, by comparing the r.h.s. of eq.(B4) and (B5) we see that p_V is identical to the virial pressure of formula (18).

Appendix C: Thermodynamic pressure in the Riddell-Uhlenbeck GCN model

We write the Kramers equation associated with eqs. (24)-(27) for the joint distribution function, P_c, of the collective variables:

$$\frac{\partial P_c(q,v,Q,V,t)}{\partial t} + v\frac{\partial}{\partial q}P_c - \frac{1}{\tau}(1+\frac{\tau}{\gamma}\Omega^2)\frac{\partial}{\partial v}vP_c - \frac{1}{\tau\gamma}\Omega^2 q\frac{\partial}{\partial v}P_c$$
$$+ V\frac{\partial}{\partial Q}P_c - \frac{1}{\tau}(1+\frac{\tau}{\gamma}\omega^2)\frac{\partial}{\partial V}VP_c - \frac{1}{\tau\gamma}\omega^2 Q\frac{\partial}{\partial V}P_c = \frac{2D}{\tau^2}\frac{\partial^2 P_c}{\partial v^2} + \frac{D}{2\tau^2}\frac{\partial^2 P_c}{\partial V^2} \qquad \text{(C1)}$$

and look for a time-independent solution whose momentum currents $j_v(q,Q) \equiv \int dvdV\,vP_c(q,v,Q,V)$ and $j_V(q,Q) \equiv \int dvdV\,VP_c(q,v,Q,V)$ vanish for all values of q and Q under the following form[37]:

$$P_c^{st}(q,Q,v,V) =$$
$$P_c^{config}(q,Q)\exp\Big\{-\frac{\tau}{D}\Big[(1+\frac{\tau}{\gamma}\omega^2)V^2 + \frac{1}{4}(1+\frac{\tau}{\gamma}\Omega^2)v^2\Big]\Big\}. \qquad \text{(C2)}$$

Substituting (C2) into eq. (C1), multiplying the latter by v and by V, integrating over velocities and imposing that currents vanish we obtain the following two equations which determine $P_c^{config}(q,Q)$:

$$\frac{1}{1+\frac{\tau}{\gamma}\Omega^2}\frac{\partial}{\partial q}P_c^{config}(q,Q) + \frac{1}{2D\gamma}\Omega^2 qP_c^{config}(q,Q) = 0 \qquad \text{(C3)}$$

$$\frac{1}{1+\frac{\tau}{\gamma}\omega^2}\frac{\partial}{\partial Q}P_c^{config}(q,Q) + \frac{2}{D\gamma}\omega^2 QP_c^{config}(q,Q) = 0 \qquad \text{(C4)}$$

which are compatible with the solution given by formula (28).

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